## 600t吊りクローラクレーン <br> DEMAG CC2800－1

| 動作速度 |  |  |  |
| :---: | :---: | :---: | :---: |
|  | 速度 | $\begin{aligned} & 1 \text { 本あたり } \\ & \text { の啟容口ー } \\ & \text { プ引腲力 } \end{aligned}$ | ロープの長さ直径 |
| ホイストH1 | $\begin{aligned} & \text { 最大 } 120 \mathrm{~m} / \text { 分 } \\ & \text { 最大 } 393.7 \mathrm{ft} / \text { 分 } \end{aligned}$ | $\begin{aligned} & 158 \mathrm{kN} \\ & 33721 \mathrm{lbf} \end{aligned}$ | $\begin{aligned} & 900 \mathrm{~m} / 28 \mathrm{~mm} \\ & 2953 \mathrm{ft} / 1.1 \mathrm{in} \end{aligned}$ |
| ホイスト H2 | $\begin{aligned} & \text { 最大 } 120 \mathrm{~m} / \text { 分 } \\ & \text { 最大 } 393.7 \mathrm{ft} / \text { 分 } \end{aligned}$ | $\begin{aligned} & 158 \mathrm{kN} \\ & 33721 \mathrm{lbf} \end{aligned}$ | $900 \mathrm{~m} / 28 \mathrm{~mm}$ $2953 \mathrm{ft} / 1.1$ in |
| 起伏装置 | 最大 $52 \mathrm{~m} /$ 分最大 $170.6 \mathrm{ft} /$ 分 |  | $\begin{aligned} & 2 \times 275 \mathrm{~m} / 30 \mathrm{~mm} \\ & 2 \times 902 \mathrm{ft} / 1.2 \mathrm{in} \end{aligned}$ |
| ラッフィングギア <br> W1／H3（OP） | 最大 $120 \mathrm{~m} /$ 分最大 $393.7 \mathrm{ft} /$ 分 |  | $800 \mathrm{~m} / 28 \mathrm{~mm}$ $2625 \mathrm{ft} / 1.1$ in |
| $\begin{aligned} & \text { ラッフィングギア } \\ & \text { W2 (オプション装 } \\ & \text { W置) } \end{aligned}$ | 最大 $120 \mathrm{~m} /$ 分最大 $393.7 \mathrm{ft} /$ 分 |  | $865 \mathrm{~m} / 28 \mathrm{~mm}$ $2838 \mathrm{ft} / 1.1 \mathrm{in}$ |
| $\begin{aligned} & \text { リービングウィン } \\ & \text { チR1 (OP) } \end{aligned}$ |  |  | $320 \mathrm{~m} / 10 \mathrm{~mm}$ $1050 \mathrm{ft} / 0.4 \mathrm{in}$ |
| 旋回装置 | $0.7 \mathrm{~min}^{-1} / 0.7 \mathrm{rpm}$ |  |  |
| 移動速度 | 1 速ギア $0 \sim 0.6 \mathrm{~km} / \mathrm{h}$ 1 速 1 ギア 0～0．37mph |  |  |
| 移動速度 | 2 速ギア $0 \sim 1.2 \mathrm{~km} / \mathrm{h}$ 2 速ギア $0 \sim 0.74 \mathrm{mph}$ |  |  |
| 移動速度 | 3 速ギア 0～1．8km／h 3 速ギア 0～1．11mph |  |  |

Basic crane dimensions • Hauptabmessungen－Dimensions de la grue de base
Basic crane dimensions with standard Superlift attachment
Hauptabmessungen mit serienmäßiger Superlifteinrichtung
Dimensions de la grue de base avec Superlift de série


## SPECIFICATIONS

## Technische Daten • Caractéristiques

Carrier performance with standard drive - Fahrleistungen bei Standard-Antrieb -
Performances du porteur au entrainement standard

```
1st gear - 1. Gang · 1ère vitesse
0-0,6 km/h
2 nd gear - 2. Gang · 2ème vitesse
0-1,2 km/h
```

Hook block system • Unterflaschensystem - Système de crochet-moufle

| Type Typ Type | Possible load Mögliche Traglast Charge possible | Number of sheaves Anzahl der Rollen Nombre de poulies | Number of lines <br> Strangzahl <br> Nombre de brins | Weight Gewicht Poids | ${ }_{\text {n }} \mathrm{D}^{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $2 \times 300$ | 600 t | $2 \times 11$ | $2 \times 22$ | $10,4 t-12,0 t$ | $5,00 \mathrm{~m}$ |
|  | 247 t | 11 | 17 | $7,1 t-7,9 t$ | $5,40 \mathrm{~m}$ |
| $2 \times 200$ | 400 t | $2 \times 7$ | $2 \times 14$ | $8,2 \mathrm{t}-10,0 \mathrm{t}$ | 5,00 m |
|  | 196 t | 7 | 13 | $5,3 \mathrm{t}-6,2 \mathrm{t}$ | $5,40 \mathrm{~m}$ |
| 160 | 160 t | 5 | 11 | $3,6 \mathrm{t} / 5,1 \mathrm{t} / 6,6 \mathrm{t}$ | 4,60 m |
|  | 125 t | $2 \times 2$ * | $2 \times 4$ | $3,6 \mathrm{t} / 5,1 \mathrm{t} / 6,6 \mathrm{t}$ | $7,10 \mathrm{~m}$ |
| 110 | 110 t | 3 | 7 | $2,3 \mathrm{t}-4,1 \mathrm{t}$ | 4,70 m |
| 50 | 50 t | 1 | 3 | $2,0 \mathrm{t}-2,8 \mathrm{t}$ | 4,00 m |
| 16 | 16 t | - | 1 | 0,9 t | $3,00 \mathrm{~m}$ |

* only on LF2 • nur an LF2 • seulement sur LF2



## Superlift-Konfigurationen • Combinaisons Superlift

Standard-SL $\qquad$ 11, 13, 15 m


Tele-SL $\leftrightarrow$ 13-17m


## BOOM COMBINATIONS

Ausleger-Kombinationen - Combinaisons de flèche



| 180 t + 60 t ZB |  |  | $\xrightarrow[-18,40 ~ m ~]{\text { m }}$ |  |  | 2 $9.8 \mathrm{~m} / \mathrm{s}$ |  |  | $360^{\circ}$ |  | EN13000 / ISO |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcup_{1}$ | $24,0 \text { m }$ | 30,0 m | 36,0 m | 42,0 m | 48,0 m | 54,0 m | 60,0 m | 66,0 m | 72,0 m | 78,0 m | 84,0 m | $\bigcup_{1 \rightarrow 1}$ |
| m | t | t | t | t | t | t | t | t | t | t | t | m |
| 6 | 600,0 | - | - | - | - | - | - | - | - | - | - | 6 |
| 7 | 561,0 | 554,0 | 567,0 | - | - | - | - | - | - | - | - | 7 |
| 8 | 506,0 | 502,0 | 499,0 | 496,0 | 494,0 | - | - | - | - | - | - | 8 |
| 9 | 410,0 | 408,0 | 407,0 | 406,0 | 405,0 | 404,0 | 404,0 | - | - | - | - | 9 |
| 10 | 337,0 | 335,0 | 334,0 | 332,0 | 331,0 | 330,0 | 330,0 | 329,0 | 301,0 | - | - | 10 |
| 12 | 247,0 | 245,0 | 243,0 | 241,0 | 240,0 | 239,0 | 239,0 | 238,0 | 237,0 | 236,0 | 212,0 | 12 |
| 14 | 193,0 | 191,0 | 190,0 | 188,0 | 186,0 | 185,0 | 185,0 | 184,0 | 183,0 | 182,0 | 181,0 | 14 |
| 16 | 158,0 | 156,0 | 154,0 | 152,0 | 151,0 | 150,0 | 149,0 | 148,0 | 147,0 | 147,0 | 145,0 | 16 |
| 18 | 133,0 | 131,0 | 129,0 | 127,0 | 126,0 | 125,0 | 124,0 | 123,0 | 122,0 | 121,0 | 120,0 | 18 |
| 20 | 115,0 | 113,0 | 111,0 | 109,0 | 107,0 | 106,0 | 105,0 | 104,0 | 103,0 | 102,0 | 101,0 | 20 |
| 22 | 101,0 | 98,5 | 96,5 | 94,5 | 93,0 | 91,5 | 90,5 | 89,5 | 88,5 | 88,0 | 86,0 | 22 |
| 24 | - | 87,5 | 85,0 | 83,0 | 81,5 | 80,0 | 79,0 | 78,0 | 77,0 | 76,0 | 74,5 | 24 |
| 26 | - | 78,0 | 76,0 | 73,5 | 72,0 | 70,5 | 69,5 | 68,5 | 67,5 | 66,5 | 65,0 | 26 |
| 28 | - | 70,5 | 68,0 | 66,0 | 64,0 | 63,0 | 61,5 | 60,5 | 59,5 | 58,5 | 57,0 | 28 |
| 30 | - | - | 62,0 | 59,5 | 57,5 | 56,5 | 55,0 | 54,0 | 53,0 | 52,0 | 50,0 | 30 |
| 34 | - | - | - | 49,5 | 47,5 | 46,1 | 44,8 | 43,6 | 42,4 | 41,2 | 39,1 | 34 |
| 38 | - | - | - | 42,1 | 39,9 | 38,3 | 36,7 | 35,2 | 33,8 | 32,6 | 30,5 | 38 |
| 42 | - | - | - | , | 34,1 | 31,9 | 30,2 | 28,7 | 27,2 | 25,9 | 23,8 | 42 |
| 46 | - | - | - | - | , | 27,0 | 25,1 | 23,4 | 21,9 | 20,6 | 18,4 | 46 |
| 50 | - | - | - | - | - | - | 21,0 | 19,3 | 17,6 | 16,2 | 14,0 | 50 |
| 54 | - | - | - | - | - | - | 17,8 | 15,9 | 14,1 | 12,6 | 10,4 | 54 |
| 58 | - | - | - | - | - | - | - | 13,2 | 11,2 | 9,7 | 7,4 | 58 |
| 62 | - | - | - | - | - | - | - | - | 8,9 | 7,2 | , | 62 |
| 66 | - | - | - | - | - | - | - | - | - | 5,2 | - | 66 |



| - | 8,40 m |  |  | 19.8 m/s |  |  | $360^{\circ}$ |  |  | EN13000 / ISO |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\circlearrowright$ | 66 m |  |  | 72 m |  |  | 78 m |  |  | 84 m |  |  |
|  | SH/LH |  | $\begin{gathered} \mathrm{SH} / \mathrm{LH} \\ \text { +SGL_S7 } \end{gathered}$ | SH/LH |  | $\begin{gathered} \mathrm{SH} / \mathrm{LH} \\ +\mathrm{SGL} \text { S } 7 \end{gathered}$ | SH/LH |  | $\begin{gathered} \mathrm{SH} / \mathrm{LH} \\ \text { +SGL_S7 } \end{gathered}$ | SH/LH |  | $\begin{gathered} \mathrm{SH} / \mathrm{LH} \\ +\mathrm{SGL} \text { S } \end{gathered}$ |
|  | 160 t | 180 t | 60 t ZB | 160 t - $180 \mathrm{t}+60 \mathrm{t}$ ZB |  |  |  |  |  | 160 t L $180 \mathrm{t}+60 \mathrm{t}$ ZB |  |  |
| m | t | t | t | t | t | t | t | t | t | t | t | t |
| 9 | 298,0 | 298,0 | - | - | - | - | - | - | - | - | - | - |
| 10 | 276,0 | 298,0 | - | 249,0 | 249,0 | - | 202,0 | 202,0 | 222,0 | - | - | - |
| 11 | 238,0 | 271,0 | - | 224,5 | 246,5 | - | 201,0 | 202,0 | 217,5 | - | - | 215,0 |
| 12 | 200,0 | 244,0 | - | 200,0 | 244,0 | - | 200,0 | 202,0 | 213,0 | 169,0 | 169,0 | 206,0 |
| 14 | 155,0 | 190,0 | - | 155,0 | 190,0 | - | 155,0 | 174,0 | 178,0 | 150,0 | 150,0 | 173,0 |
| 16 | 126,0 | 154,0 | - | 125,0 | 154,0 | - | 125,0 | 153,0 | 153,0 | 124,0 | 133,0 | 148,0 |
| 18 | 104,0 | 129,0 | - | 104,0 | 129,0 | - | 104,0 | 129,0 | 128,0 | 103,0 | 119,0 | 126,0 |
| 20 | 89,0 | 110,0 | - | 88,5 | 110,0 | - | 88,5 | 110,0 | 109,0 | 87,5 | 107,0 | 107,0 |
| 22 | 76,5 | 96,0 | - | 76,5 | 95,5 | - | 76,0 | 95,0 | 94,0 | 75,0 | 94,5 | 93,0 |
| 24 | 67,0 | 84,0 | - | 66,5 | 84,0 | - | 66,0 | 83,5 | 82,5 | 65,5 | 82,5 | 81,0 |
| 26 | 59,0 | 74,5 | - | 58,5 | 74,0 | - | 58,0 | 74,0 | 72,5 | 57,5 | 73,0 | 71,5 |
| 28 | 52,5 | 66,5 | - | 52,0 | 66,5 | - | 51,5 | 66,0 | 65,0 | 50,5 | 65,0 | 63,5 |
| 30 | 47,0 | 60,0 | - | 46,6 | 59,5 | - | 46,2 | 59,0 | 58,0 | 45,3 | 58,5 | 56,5 |
| 34 | 38,1 | 49,5 | - | 37,7 | 49,1 | - | 37,3 | 48,7 | 47,5 | 36,3 | 47,8 | 46,2 |
| 38 | 31,3 | 41,5 | - | 30,8 | 41,0 | - | 30,2 | 40,5 | 39,3 | 29,1 | 39,6 | 37,9 |
| 42 | 25,7 | 35,1 | - | 25,1 | 34,6 | - | 24,6 | 34,1 | 32,7 | 23,4 | 33,0 | 31,1 |
| 46 | 21,2 | 29,9 | - | 20,6 | 29,3 | - | 20,0 | 28,7 | 27,2 | 18,8 | 27,5 | 25,6 |
| 50 | 17,6 | 25,5 | - | 16,9 | 24,8 | - | 16,3 | 24,2 | 22,7 | 15,1 | 23,0 | 21,1 |
| 54 | 14,6 | 21,9 | - | 13,9 | 21,2 | - | 13,2 | 20,5 | 19,0 | 12,0 | 19,3 | 17,3 |
| 58 | 12,2 | 18,9 | - | 11,3 | 18,1 | - | 10,6 | 17,4 | 15,8 | 9,4 | 16,1 | 14,2 |
| 62 | , | - | - | 9,2 | 15,5 | - | 8,4 | 14,7 | 13,2 | 7,2 | 13,5 | 11,5 |
| 66 | - | - | - | - | , | - | 6,6 | 12,5 | 10,9 | 5,3 | 11,2 | 9,2 |
| 70 | - | - | - | - | - | - | 5,1 | 10,6 | 9,0 | - | 9,2 | 7,2 |
| 74 | - | - | - | - | - | - | , | , | , | - | 7,6 | 5,5 |
| 75 | - | - | - | - | - | - | - | - | - | - | - | 5,2 |



For SH/LH+SGL_S7 a boom power-kit is required • Für SH/LH+SGL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich •
Un kit à fortifier de flèche principale est nécessaire pour SH/LH+SGL_S7




For HSSL_S7 a boom power-kit is required • Für HSSL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich .
Un kit à fortifier de flèche principale est nécessaire pour HSSL_S7


For HSSL_S7 a boom power-kit is required • Für HSSL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich •
Un kit à fortifier de flèche principale est nécessaire pour HSSL_S7


For HSSL_S7 a boom power-kit is required • Für HSSL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich •
Un kit à fortifier de flèche principale est nécessaire pour HSSL_S7


For SSL/LSL+SGL_S7 a boom power-kit is required • Für SSL/LSL+SGL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich Un kit à fortifier de flèche principale est nécessaire pour SSL/LSL+SGL_S7


For SSL/LSL+SGL_S7 a boom power-kit is required • Für SSL/LSL+SGL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich •
Un kit à fortifier de flèche principale est nécessaire pour SSL/LSL+SGL_S7


| \% |  | 60 m |  |  | 66 m |  |  | 72 m |  |  | 78 m |  |  | 84 m |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ |  |
| m | , | t | t | t | t | t | t | t | t | t | t | t | t | t | t |  |
| 26 | 83,5 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |  |
| 28 | 75,5 | - | - | 75,0 | - | - | - | - | - | - | - | - | - | - | - |  |
| 30 | 68,5 | - | - | 68,0 | - | - | 67,0 | - | - | - | - | - | - | - | - |  |
| 34 | 57,5 | - | - | 57,0 | - | - | 56,0 | - | - | 55,5 | - | - | 54,5 | - | - |  |
| 38 | 49,4 | - | - | 48,7 | - | - | 47,5 | - | - | 47,3 | - | - | 46,4 | - | - |  |
| 40 | 46,0 | 41,5 | - | 45,4 | - | - | 44,2 | - | - | 44,0 | - | - | 43,0 | - | - |  |
| 42 | 42,7 | 38,6 | - | 42,1 | - | - | 40,9 | - | - | 40,7 | - | - | 39,7 | - | - |  |
| 44 | 40,0 | 36,0 | - | 39,4 | 35,2 | - | 38,2 | - | - | 38,0 | - | - | 37,0 | - | - |  |
| 46 | 37,4 | 33,7 | - | 36,7 | 32,9 | - | 35,6 | 31,6 | - | 35,3 | - | - | 34,4 | - | - |  |
| 50 | 33,0 | 29,6 | - | 32,3 | 28,8 | - | 31,2 | 27,5 | - | 30,9 | 27,0 | - | 30,0 | - | - |  |
| 52 | 31,1 | 27,8 | - | 30,5 | 27,0 | - | 29,3 | 25,6 | - | 29,0 | 25,2 | - | 28,1 | 24,0 | - |  |
| 54 | 29,3 | 26,2 | 22,7 | 28,7 | 25,3 | - | 27,5 | 23,9 | - | 27,2 | 23,5 | - | 26,3 | 22,3 | - |  |
| 58 | 26,3 | 23,2 | 19,9 | 25,6 | 22,3 | 18,9 | 24,4 | 20,8 | - | 24,1 | 20,4 | - | 23,0 | 19,2 | - |  |
| 62 | 23,6 | 20,6 | 17,5 | 22,9 | 19,7 | 16,5 | 21,6 | 18,2 | 15,0 | 21,3 | 17,8 | - | 20,2 | 16,6 | - |  |
| 66 | , | 18,4 | 15,5 | 20,6 | 17,5 | 14,5 | 19,2 | 16,0 | 13,0 | 18,8 | 15,5 | 12,4 | 17,7 | 14,4 | - |  |
| 68 | - | 17,4 | 14,6 | , | 16,5 | 13,6 | 18,1 | 15,0 | 12,0 | 17,7 | 14,5 | 11,5 | 16,6 | 13,4 | - |  |
| 70 | - | , | 13,7 | - | 15,5 | 12,7 | 17,1 | 14,1 | 11,2 | 16,6 | 13,6 | 10,7 | 15,6 | 12,4 | 9,4 |  |
| 74 | - | - | , | - | 13,9 | 11,2 | 15,3 | 12,4 | 9,6 | 14,8 | 11,9 | 9,1 | 13,7 | 10,7 | 7,8 |  |
| 78 | - | - | - | - | , | 9,9 | , | 10,9 | 8,3 | 13,2 | 10,4 | 7,7 | 12,0 | 9,2 | 6,5 |  |
| 80 | - | - | - | - | - | - | - | 10,3 | 7,7 | - | 9,7 | 7,1 | 11,3 | 8,5 | 5,8 |  |
| 82 | - | - | - | - | - | - | - | , | 7,1 | - | 9,0 | 6,5 | 10,6 | 7,8 | 5,2 |  |
| 84 | - | - | - | - | - | - | - | - | , | - | 8,4 | 5,9 | 9,9 | 7,2 | 4,7 |  |
| 86 | - | - | - | - | - | - | - | - | - | - | - | 5,4 | 9,3 | 6,7 | 4,2 |  |
| 90 | - | - | - | - | - | - | - | - | - | - | - | 4,5 | - | 5,6 | - |  |

Main boom angle $85^{\circ}, 75^{\circ}$ and $65^{\circ}$, capacities for intermediate boom positions are calculated by the crane control system IC-1
Hauptauslegerwinkel $85^{\circ}$, $75^{\circ}$ und $65^{\circ}$, Traglasten für Zwischenstellungen des Hauptauslegers werden von der Kransteuerung IC-1 berechnet Jarret de flèche principale $85^{\circ}, 75^{\circ}$ et $65^{\circ}$, le système de commande de la grue IC - 1 calcule les charges pour les positions intermédiaires de la flèche


| \% | 60 m |  |  | 66 m |  |  | 72 m |  |  | 78 m |  |  | 84 m |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\xrightarrow{0}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ |  |  |
| m | t | t | t | t | t | t | t | t | t | t | t | t | t | t | t |  |  |
| 26 | 82,0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |  |  |
| 28 | 74,0 | - | - | 73,5 | - | - | - | - | - | - | - | - | - | - | - |  |  |
| 30 | 67,0 | - | - | 66,5 | - | - | 65,5 | - | - | - | - | - | - | - | - |  |  |
| 34 | 56,5 | - | - | 55,5 | - | - | 54,5 | - | - | 54,0 | - | - | 53,0 | - | - |  |  |
| 38 | 48,2 | - | - | 47,5 | - | - | 46,4 | - | - | 46,1 | - | - | 45,2 | - | - |  |  |
| 42 | 41,7 | - | - | 41,0 | - | - | 39,8 | - | - | 39,6 | - | - | 38,6 | - | - |  |  |
| 44 | 39,0 | 33,0 | - | 38,3 | - | - | 37,2 | - | - | 36,9 | - | - | 36,0 | - | - |  |  |
| 46 | 36,4 | 30,7 | - | 35,7 | 29,7 | - | 34,6 | - | - | 34,3 | - | - | 33,4 | - | - |  |  |
| 50 | 32,1 | 26,7 | - | 31,4 | 25,7 | - | 30,2 | 24,1 | - | 30,0 | - | - | 29,0 | - | - |  |  |
| 52 | 30,3 | 24,9 | - | 29,6 | 23,9 | - | 28,4 | 22,4 | - | 28,1 | 22,0 | - | 27,1 | - | - |  |  |
| 54 | 28,5 | 23,3 | - | 27,8 | 22,3 | - | 26,6 | 20,8 | - | 26,3 | 20,4 | - | 25,3 | 19,1 | - |  |  |
| 58 | 25,4 | 20,4 | - | 24,7 | 19,5 | - | 23,5 | 18,0 | - | 23,1 | 17,5 | - | 22,0 | 16,3 | - |  |  |
| 62 | 22,8 | 18,0 | 13,3 | 22,1 | 17,0 | 12,3 | 20,7 | 15,5 | - | 20,3 | 15,1 | - | 19,2 | 13,9 | - |  |  |
| 66 | - | 15,9 | 11,5 | 19,7 | 14,9 | 10,5 | 18,3 | 13,4 | 8,8 | 17,9 | 13,0 | - | 16,8 | 11,8 | - |  |  |
| 70 | - | 14,1 | 9,9 | 17,7 | 13,1 | 8,9 | 16,2 | 11,6 | 7,3 | 15,8 | 11,1 | 6,7 | 14,7 | 9,9 | - |  |  |
| 74 | - | - | 8,6 | - | 11,6 | 7,5 | 14,4 | 10,0 | 5,9 | 13,9 | 9,5 | 5,4 | 12,8 | 8,3 | - |  |  |
| 76 | - | - | 8,0 | - | 10,9 | 6,9 | - | 9,3 | 5,3 | 13,1 | 8,8 | 4,7 | 12,0 | 7,6 | - |  |  |
| 78 | - | - | 7,4 | - | - | 6,3 | - | 8,7 | 4,7 | 12,3 | 8,1 | 4,2 | 11,2 | 6,9 | - |  |  |
| 80 | - | - | - | - | - | 5,8 | - | 8,0 | 4,2 | - | 7,5 | - | 10,5 | 6,3 | - |  |  |
| 82 | - | - | - | - | - | 5,3 | - | 7,5 | - | - | 6,9 | - | 9,8 | 5,7 | - |  |  |
| 86 | - | - | - | - | - | - | - | - | - | - | 5,8 | - | 8,5 | 4,6 | - |  |  |
| 88 | - | - | - | - | - | - | - | - | - | - | 5,3 | - | - | 4,1 | - |  |  |

Main boom angle $85^{\circ}, 75^{\circ}$ and $65^{\circ}$, capacities for intermediate boom positions are calculated by the crane control system IC-1
Hauptauslegerwinkel $85^{\circ}, 75^{\circ}$ und $65^{\circ}$, Traglasten für Zwischenstellungen des Hauptauslegers werden von der Kransteuerung IC-1 berechnet Jarret de flèche principale $85^{\circ}, 75^{\circ}$ et $65^{\circ}$, le système de commande de la grue IC-1 calcule les charges pour les positions intermédiaires de la flèche


Main boom angle $85^{\circ}, 75^{\circ}$ and $65^{\circ}$, capacities for intermediate boom positions are calculated by the crane control system IC-1
Hauptauslegerwinkel $85^{\circ}$, $75^{\circ}$ und $65^{\circ}$, Traglasten für Zwischenstellungen des Hauptauslegers werden von der Kransteuerung IC- 1 berechnet Jarret de flèche principale $85^{\circ}, 75^{\circ}$ et $65^{\circ}$, le système de commande de la grue IC - 1 calcule les charges pour les positions intermédiaires de la flèche


Main boom angle $85^{\circ}, 75^{\circ}$ and $65^{\circ}$, capacities for intermediate boom positions are calculated by the crane control system IC-1
Hauptauslegerwinkel $85^{\circ}, 75^{\circ}$ und $65^{\circ}$, Traglasten für Zwischenstellungen des Hauptauslegers werden von der Kransteuerung IC-1 berechnet Jarret de flèche principale $85^{\circ}, 75^{\circ}$ et $65^{\circ}$, le système de commande de la grue IC-1 calcule les charges pour les positions intermédiaires de la flèche



| $36 \mathrm{~m}+36 \mathrm{~m}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| m | t | t | t | t | t | t | t |
| 18 | 154,0 | 257,0 | - | - | - | - | - |
| 20 | 133,0 | 257,0 | - | - | - | 253,0 | - |
| 22 | 117,0 | 253,0 | - | - | - | 249,0 | - |
| 24 | 104,0 | 239,0 | - | - | - | 245,0 | - |
| 26 | 93,5 | 226,0 | - | - | - | 239,0 | - |
| 28 | 85,0 | 208,0 | - | - | - | 224,0 | - |
| 30 | 77,5 | 187,0 | 199,0 | - | - | 208,0 | - |
| 34 | 65,5 | 152,0 | 183,0 | - | - | 185,0 | - |
| 38 | 56,5 | 123,0 | 165,0 | - | - | 161,0 | - |
| 42 | - | - | 146,0 | 141,0 | - | 142,0 | - |
| 46 | - | - | 118,0 | 128,0 | - | 126,0 | - |
| 50 | - | - | - | 116,0 | - | 112,0 | - |
| 52 | - | - | - | 111,0 | 107,0 | 106,5 | - |
| 54 | - | - | - | - | 102,0 | 101,0 | - |
| 58 | - | - | - | - | 94,5 | 87,0 | - |
| 62 | - | - | - | - | - | 76,0 | - |
| 66 | - | - | - | - | - | 66,0 | - |


|  | $36 \mathrm{~m}+$ | $\mathbf{4 8} \mathbf{m}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| m | t | t | t | t | t | t | t |
| 22 | 115,0 | 187,0 | - | - | - | - | - |
| 24 | 102,0 | 187,0 | - | - | - | 186,0 | - |
| 26 | 92,0 | 187,0 | - | - | - | 185,0 | - |
| 28 | 83,0 | 180,0 | - | - | - | 183,0 | - |
| 30 | 75,5 | 172,0 | - | - | - | 181,0 | - |
| 34 | 64,0 | 156,0 | - | - | - | 164,0 | - |
| 36 | 59,5 | 146,0 | 153,0 | - | - | 156,5 | - |
| 38 | 55,0 | 136,0 | 153,0 | - | - | 149,0 | - |
| 42 | 48,0 | 116,0 | 135,0 | - | - | 138,0 | - |
| 46 | 42,4 | 99,5 | 120,0 | - | - | 126,0 | - |
| 50 | 37,7 | 84,0 | 109,0 | 112,0 | - | 113,0 | - |
| 54 | - | - | 97,5 | 104,0 | - | 102,0 | - |
| 58 | - | - | 82,0 | 95,5 | - | 92,0 | - |
| 60 | - | - | - | 91,5 | 86,5 | 88,0 | - |
| 62 | - | - | - | 88,0 | 85,0 | 84,0 | - |
| 64 | - | - | - | 84,5 | 82,0 | 79,0 | - |
| 66 | - | - | - | - | 79,0 | 74,0 | - |
| 68 | - | - | - | - | 76,0 | 69,0 | - |
| 70 | - | - | - | - | - | 64,0 | - |
| 74 | - | - | - | - | - | 58,0 | - |
| 78 | - | - | - | - | - | 49,0 | - |


| $36 \mathrm{~m}+60 \mathrm{~m}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\underset{1}{\bigcup}$ | SWSL |  |  |  |  | SFSL | $\begin{aligned} & \text { HSWSL } \\ & -\mathrm{S} 7 \end{aligned}$ |
|  | 曰 0 t | $0 \mathrm{t}-250 \mathrm{t}$ |  |  |  |  |  |
|  | $\begin{aligned} & 180 \mathrm{t}+ \\ & \\ & 60 \mathrm{tZB} \end{aligned}$ |  |  |  |  |  |  |
|  | - $85^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $55^{\circ}$ |  | $85^{\circ}$ |
| m | t | t | t | t | t | t | t |
| 26 | 90,0 | 134,0 | - | - | - | - | - |
| 28 | 81,5 | 134,0 | - | - | - | 134,0 | - |
| 30 | 74,0 | 134,0 | - | - | - | 133,0 | - |
| 34 | 62,0 | 128,0 | - | - | - | 133,0 | - |
| 38 | 53,0 | 119,0 | - | - | - | 130,0 | - |
| 42 | 46,3 | 110,0 | 117,0 | - | - | 124,0 | - |
| 46 | 40,6 | 100,0 | 112,0 | - | - | 116,0 | - |
| 50 | 35,9 | 90,0 | 102,0 | - | - | 105,0 | - |
| 54 | 32,0 | 78,5 | 96,0 | - | - | 94,0 | - |
| 56 | 30,3 | 73,5 | 93,0 | 86,5 | - | 90,0 | - |
| 58 | 28,7 | 68,5 | 88,5 | 86,5 | - | 86,0 | - |
| 62 | 25,9 | 58,5 | 78,0 | 80,0 | - | 81,0 | - |
| 66 | - | - | 68,0 | 73,5 | - | 76,0 | - |
| 70 | - | - | 58,0 | 68,5 | 68,5 | 70,0 | - |
| 74 | - | - | - | 63,5 | 65,5 | 62,0 | - |
| 76 | - | - | - | 61,0 | 63,0 | 58,5 | - |
| 78 | - | - | - | - | 61,0 | 55,0 | - |
| 80 | - | - | - | - | 58,5 | 52,0 | - |
| 82 | - | - | - | - | - | 50,0 | - |
| 86 | - | - | - | - | - | 43,0 | - |
| 90 | - | - | - | - | - | 37,0 | - |


| $36 \mathrm{~m}+72 \mathrm{~m}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| m | t | t | t | t | t | t | t |
| 30 | 72,0 | 96,0 | - | - | - | - | - |
| 34 | 60,5 | 96,0 | - | - | - | 95,0 | - |
| 38 | 51,5 | 94,0 | - | - | - | 94,0 | - |
| 42 | 44,4 | 91,0 | - | - | - | 93,0 | - |
| 46 | 38,7 | 87,0 | - | - | - | 91,0 | - |
| 48 | 36,3 | 85,0 | 87,0 | - | - | 89,5 | - |
| 50 | 34,0 | 83,0 | 86,0 | - | - | 88,0 | - |
| 54 | 30,1 | 79,0 | 84,0 | - | - | 83,0 | - |
| 58 | 26,8 | 72,0 | 81,0 | - | - | 78,0 | - |
| 62 | 23,9 | 64,0 | 78,0 | - | - | 73,0 | - |
| 64 | 22,6 | 60,2 | 75,5 | 67,0 | - | 70,5 | - |
| 66 | 21,3 | 56,5 | 71,5 | 66,5 | - | 68,0 | - |
| 70 | 19,1 | 49,8 | 64,0 | 64,0 | - | 64,0 | - |
| 74 | 17,2 | 42,8 | 57,0 | 60,5 | - | 61,0 | - |
| 78 | - | - | 50,0 | 57,5 | 57,5 | 57,0 | - |
| 80 | - | - | 46,8 | 56,0 | 55,5 | 54,5 | - |
| 82 | - | - | - | 54,0 | 54,0 | 52,0 | - |
| 86 | - | - | - | 49,8 | 50,0 | 46,0 | - |
| 90 | - | - | - |  | 47,1 | 42,0 | - |
| 92 | - | - | - | - | 45,6 | 39,5 | - |
| 94 | - | - | - | - | - | 37,0 | - |
| 98 | - | - | - | - | - | 32,0 | - |
| 102 | - | - | - | - | - | 28,0 | - |

Main boom angle $85^{\circ}, 75^{\circ}, 65^{\circ}$ and $55^{\circ}$; capacities for intermediate boom positions are calculated by the crane control system IC-1
Hauptauslegerwinkel $85^{\circ}, 75^{\circ}, 65^{\circ}$ und $55^{\circ}$; Traglasten für Zwischenstellungen des Hauptauslegers werden von der Kransteuerung IC-1 berechnet
Jarret de flèche principale $85^{\circ}, 75^{\circ}, 65^{\circ}$ et $55^{\circ}$; le système de commande de la grue IC-1 calcule les charges pour les positions intermédiaires de la flèche

For HSWSL_S7 a boom power-kit is required!
Für HSWSL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich! Un kit à fortifier de flèche principale est nécessaire pour HSWSL_S7!

|  | - 8,40 |  |  | 11-15 m |  |  | $19.8 \mathrm{~m} / \mathrm{s}$ |  | $360^{\circ}$ |  |  |  | EN13000 / ISO |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $36 m+84 m$ |  |  |  |  |  |  |  | $48 \mathrm{~m}+36 \mathrm{~m}$ |  |  |  |  |  |  |  |
| $\bigcup_{1}$ | SWSL 0 (t-250t SFSL ${ }_{\text {HSWSL }}^{\text {HSW7 }}$ |  |  |  |  |  |  |  |  | SWSL |  |  |  | $\text { SFSL } \begin{gathered} \text { HSWSL } \\ -\mathrm{S} 7 \end{gathered}$ |  |
|  |  |  |  |  |  |  |  | L $0 \mathrm{t}-250 \mathrm{t}$ |
|  | $\begin{aligned} & 180 t+ \\ & 60 t \mathrm{ZB} \end{aligned}$ | 160 t |  |  |  |  |  |  |  |  | 160 t |  |  | $85^{\circ}$ |  |
|  | $85^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $55^{\circ}$ |  | $85^{\circ}$ |  |  |  |  |  |  |  |
| m | t | t | t | t | t | t | t |  |  | m | t | t | t | t | t | t | t |
| 34 | 59,0 | 69,0 | - | - | - | - | - | 20 | 131,0 |  | 223,0 | - | - | - | - | - |
| 38 | 50,0 | 69,0 | - | - | - | 69,0 | - | 22 | 115,0 | 219,0 | - | - | - | 221,0 | - |
| 42 | 43,3 | 68,0 | - | - | - | 68,0 | - | 24 | 102,0 | 212,0 | - | - | - | 219,0 | - |
| 46 | 37,6 | 68,0 | - | - | - | 68,0 | - | 26 | 92,0 | 203,0 | - | - | - | 218,0 | - |
| 50 | 32,9 | 67,0 | - | - | - | 67,0 | - | 28 | 83,5 | 194,0 | - | - | - | 216,0 | - |
| 54 | 28,9 | 66,0 | 63,0 | - | - | 66,0 | - | 30 | 76,0 | 185,0 | - | - | - | 206,0 | - |
| 58 | 25,5 | 65,0 | 63,0 | - | - | 64,0 | - | 34 | 64,5 | 159,0 | 183,0 | - | - | 184,0 | - |
| 62 | 22,5 | 63,0 | 62,0 | - | - | 62,0 | - | 38 | 55,5 | 129,0 | 162,0 | - | - | 159,0 | - |
| 66 | 19,9 | 59,0 | 61,0 | - | - | 60,0 | - | 42 | - | - | 144,0 | - | - | 139,0 | - |
| 70 | 17,6 | 53,0 | 60,0 | - | - | 57,0 | - | 46 | - | - | 129,0 | - | - | 123,0 | - |
| 72 | 16,5 | 50,2 | 59,0 | 50,0 | - | 56,0 | - | 48 | - | - | 123,0 | 117,0 | - | 116,0 | - |
| 74 | 15,5 | 47,4 | 58,5 | 50,0 | - | 55,0 | - | 50 | - | - | 109,0 | 111,0 | - | 109,0 | - |
| 78 | 13,8 | 42,2 | 53,0 | 49,9 | - | 52,0 | - | 54 | - | - | - | 102,0 | - | 98,0 | - |
| 82 | 12,2 | 37,2 | 47,8 | 48,4 | - | 50,0 | - | 56 | - | - | - | 97,5 | - | 93,5 | - |
| 86 | 10,9 | 31,9 | 42,8 | 46,7 | - | 46,0 | - | 58 | - | - | - | - | 89,5 | 89,0 | - |
| 88 | - | - | 40,3 | 45,8 | 44,1 | 44,5 | - | 62 | - | - | - | - | 82,5 | 81,0 | - |
| 90 | - | - | 37,9 | 44,7 | 44,1 | 43,0 | - | 64 | - | - | - | - | 79,5 | 77,5 | - |
| 92 | - | - | 35,3 | 43,6 | 43,7 | 41,0 | - | 66 | - | - | - | - | - | 74,0 | - |
| 94 | - | - | - | 42,5 | 42,3 | 39,0 | - | 70 | - | - | - | - | - | 67,0 | - |
| 98 | - | - | - | 37,9 | 39,5 | 36,0 | - | 74 | - | - | - | - | - | 57,0 | - |
| 102 | - | - | - | - | 37,1 | 32,0 | - | 78 | - | - | - | - | - | 51,0 | - |



[^0] flèche

For HSWSL_S7 a boom power-kit is required!
Für HSWSL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich!
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Main boom angle $85^{\circ}, 75^{\circ}, 65^{\circ}$ and $55^{\circ}$; capacities for intermediate boom positions are calculated by the crane control system IC-1
Hauptauslegerwinkel $85^{\circ}, 75^{\circ}, 65^{\circ}$ und $55^{\circ}$; Traglasten für Zwischenstellungen des Hauptauslegers werden von der Kransteuerung IC-1 berechnet

Jarret de flèche principale $85^{\circ}, 75^{\circ}, 65^{\circ}$ et $55^{\circ}$; le système de commande de la grue IC-1 calcule les charges pour les positions intermédiaires de la flèche
$9.8 \mathrm{~m} / \mathrm{s} \quad 360^{\circ} \quad$ EN13000/ISO

## - $48 \mathrm{~m}+84 \mathrm{~m}$



 $\mathbf{6 0 m} \mathbf{m}$

For HSWSL_S7 a boom power-kit is required!
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Main boom angle $85^{\circ}, 75^{\circ}, 65^{\circ}$ and $55^{\circ}$; capacities for intermediate boom positions are calculated by the crane control system IC-1
Hauptauslegerwinkel $85^{\circ}, 75^{\circ}, 65^{\circ}$ und $55^{\circ}$; Traglasten für Zwischenstellungen des Hauptauslegers werden von der Kransteuerung IC-1 berechnet
Jarret de flèche principale $85^{\circ}, 75^{\circ}, 65^{\circ}$ et $55^{\circ}$; le système de commande de la grue IC-1 calcule les charges pour les positions intermédiaires de la flèche

| $60 \mathrm{~m}+60 \mathrm{~m}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcup_{1}$ | SWSL |  |  |  |  | SFSL | $\begin{aligned} & \text { HSWSL } \\ & \quad-\mathrm{S} 7 \end{aligned}$ |
|  | $\boxminus 0 \mathrm{t}$ |  | $0 \mathrm{t}-250 \mathrm{t}$ |  |  |  |  |
|  | $\rightleftharpoons \begin{aligned} & 180 \mathrm{t}+ \\ & 60 \mathrm{t} \mathrm{ZB} \end{aligned}$ |  | 160 t |  |  |  | $85^{\circ}$ |
|  | - $85^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $55^{\circ}$ |  |  |
| m | t | t | t | t | t | t | t |
| 28 | 78,0 | 102,0 | - | - | - | - | 109,0 |
| 30 | 70,5 | 102,0 | - | - | - | 102,0 | 108,0 |
| 34 | 59,0 | 101,0 | - | - | - | 102,0 | 104,0 |
| 38 | 50,5 | 98,0 | - | - | - | 102,0 | 99,5 |
| 42 | 43,9 | 95,0 | - | - | - | 101,0 | 93,0 |
| 46 | 38,4 | 91,0 | - | - | - | 100,0 | 86,5 |
| 48 | 36,1 | 88,5 | 96,0 | - | - | 100,0 | 83,2 |
| 50 | 33,8 | 86,0 | 96,0 | - | - | 100,0 | 80,0 |
| 54 | 30,0 | 82,0 | 94,0 | - | - | 93,0 | 75,0 |
| 58 | 26,8 | 73,0 | 90,0 | - | - | 87,0 | 70,0 |
| 62 | 24,1 | 63,0 | 84,0 | - | - | 79,0 | 63,0 |
| 65 | - | - | 79,2 | - | - | 73,7 | 55,0 |
| 66 | - | - | 77,5 | 72,0 | - | 72,0 | , |
| 70 | - | - | 72,0 | 66,5 | - | 65,0 | - |
| 74 | - | - | 63,0 | 62,0 | - | 60,0 | - |
| 76 | - | - | 58,0 | 60,0 | - | 57,0 | - |
| 78 | - | - | - | 58,0 | - | 54,0 | - |
| 82 | - | - | - | 54,5 | - | 50,0 | - |
| 84 | - | - | - | 53,0 | 48,6 | 48,0 | - |
| 86 | - | - | - | 51,0 | 47,2 | 46,0 | - |
| 90 | - | - | - | , | 44,4 | 42,0 | - |
| 94 | - | - | - | - | 41,9 | 38,0 | - |
| 98 | - | - | - | - | - | 35,0 | - |
| 102 | - | - | - | - | - | 30,0 | - |
| 106 | - | - | - | - | - | 26,0 | - |
| 110 | - | - | - | - | - | 22,0 | - |


| $\mathbf{m}$ | $\mathbf{6 0} \mathbf{m} \mathbf{+}$ | $\mathbf{7 2 ~ m}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 32 | t | t | t | t | t | t | t |
| 34 | 57,5 | 77,0 | - | - | - | 77,0 | 78,5 |
| 38 | 48,8 | 76,0 | - | - | - | 77,0 | 76,0 |
| 42 | 42,0 | 74,0 | - | - | - | 77,0 | 73,5 |
| 46 | 36,5 | 72,0 | - | - | - | 76,0 | 71,0 |
| 50 | 31,9 | 70,0 | - | - | - | 75,0 | 68,0 |
| 54 | 28,1 | 68,0 | 71,0 | - | - | 74,0 | 65,0 |
| 58 | 24,7 | 66,0 | 71,0 | - | - | 72,0 | 62,0 |
| 62 | 21,8 | 63,0 | 71,0 | - | - | 69,0 | 59,0 |
| 66 | 19,3 | 59,5 | 69,0 | - | - | 65,0 | 56,0 |
| 70 | 17,1 | 52,5 | 64,0 | - | - | 62,0 | 52,5 |
| 74 | 15,2 | 45,9 | 60,0 | 56,0 | - | 58,0 | 45,9 |
| 77 | - | - | 57,0 | 55,7 | - | 55,0 | 40,4 |
| 78 | - | - | 56,0 | 55,5 | - | 54,0 | - |
| 82 | - | - | 52,0 | 52,0 | - | 50,0 | - |
| 86 | - | - | 46,6 | 49,0 | - | 46,0 | - |
| 90 | - | - | - | 46,1 | - | 42,0 | - |
| 92 | - | - | - | 44,7 | 40,1 | 40,0 | - |
| 94 | - | - | - | 43,4 | 38,9 | 38,0 | - |
| 96 | - | - | - | 42,3 | 37,7 | 36,5 | - |
| 98 | - | - | - | - | 36,6 | 35,0 | - |
| 102 | - | - | - | - | 34,5 | 32,0 | - |
| 106 | - | - | - | - | 32,6 | 29,0 | - |
| 110 | - | - | - | - | - | 25,0 | - |
| 114 | - | - | - | - | - | 21,0 | - |
| 118 | - | - | - | - | - | 17,0 | - |
| 122 | - | - | - | - | - | 15,0 | - |

For HSWSL_S7 a boom power-kit is required!
Für HSWSL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich! Un kit à fortifier de flèche principale est nécessaire pour HSWSL_S7!


Main boom angle $85^{\circ}, 75^{\circ}, 65^{\circ}$ and $55^{\circ}$; capacities for intermediate boom positions are calculated by the crane control system IC-1
Hauptauslegerwinkel $85^{\circ}, 75^{\circ}, 65^{\circ}$ und $55^{\circ}$; Traglasten für Zwischenstellungen des Hauptauslegers werden von der Kransteuerung IC-1 berechnet Jarret de flèche principale $85^{\circ}, 75^{\circ}, 65^{\circ}$ et $55^{\circ}$; le système de commande de la grue $\mathrm{IC}-1$ calcule les charges pour les positions intermédiaires de la flèche

For HSWSL_S7 a boom power-kit is required!
Für HSWSL_S7 ist ein Ausleger-Verstärkungs-Kit erforderlich!
Un kit à fortifier de flèche principale est nécessaire pour HSWSL_S7!

| 다- $8,40 \mathrm{~m}$ |  |  |  | 11-15 m |  | $19.8 \mathrm{~m} / \mathrm{s}$ |  |  | $360^{\circ}$ |  |  | EN13000 / ISO |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $84 \mathrm{~m}+72 \mathrm{~m}$ |  |  |  |  |  |  |  | $84 m+84 m$ |  |  |  |  |  |  |  |
| $\bigcup_{1}$ | SWSL 0 t-250t |  |  |  |  |  |  |  |  | SWSL |  |  |  | $\text { SFSL } \begin{gathered} \text { HSWSL } \\ \stackrel{-S}{-S 7} \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  | 50 t |  |  |
|  | $\begin{aligned} & 180 \mathrm{t}+ \\ & 60 \mathrm{tZB} \end{aligned}$ | 160 t |  |  |  |  |  |  |  | 160 |  |  |  |  |  |
|  | $85^{\circ}$ | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $55^{\circ}$ |  | $85^{\circ}$ |  |  | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $55^{\circ}$ |  | $85^{\circ}$ |
| m | t | t | t | t | t | t | t |  |  | m | t | t | t | t | t | t | t |
| 34 | 48,0 | 49,0 | - | - | - | - | 58,5 | 37 | - | - | - | - | - | - | 44,5 |
| 38 | 45,4 | 49,0 | - | - | - | 48,0 | 57,5 | 38 | 38,0 | 40,0 | - | - | - | - | 44,5 |
| 42 | 38,9 | 48,0 | - | - | - | 48,0 | 55,5 | 42 | 36,7 | 40,0 | - | - | - | 38,0 | 43,8 |
| 46 | 33,6 | 47,0 | - | - | - | 48,0 | 54,0 | 46 | 31,6 | 39,0 | - | - | - | 38,0 | 42,9 |
| 50 | 29,0 | 45,0 | - | - | - | 48,0 | 52,5 | 50 | 27,3 | 38,0 | - | - | - | 38,0 | 41,9 |
| 54 | 25,2 | 44,0 | - | - | - | 48,0 | 50,5 | 54 | 23,8 | 37,0 | - | - | - | 38,0 | 40,8 |
| 58 | 22,0 | 42,0 | - | - | - | 48,0 | 49,0 | 58 | 20,6 | 36,0 | - | - | - | 38,0 | 39,6 |
| 60 | 20,6 | 41,5 | 47,0 | - | - | 48,0 | 48,1 | 62 | 17,8 | 35,0 | - | - | - | 38,0 | 38,5 |
| 62 | 19,2 | 41,0 | 47,0 | - | - | 48,0 | 47,2 | 66 | 15,4 | 34,0 | 37,0 | - | - | 38,0 | 37,3 |
| 66 | 16,8 | 39,0 | 46,0 | - | - | 46,0 | 45,5 | 70 | 13,3 | 33,0 | 37,0 | - | - | 37,0 | 36,1 |
| 70 | 14,7 | 38,0 | 46,0 | - | - | 45,0 | 43,7 | 74 | 11,4 | 32,0 | 37,0 | - | - | 37,0 | 34,9 |
| 74 | 12,9 | 37,0 | 45,0 | - | - | 44,0 | 42,0 | 78 | 9,8 | 31,0 | 37,0 | - | - | 36,0 | 33,7 |
| 78 | 11,4 | 36,0 | 44,0 | - | - | 42,0 | 40,3 | 82 | 8,4 | 29,0 | 36,0 | - | - | 35,0 | 32,5 |
| 79 | - | - | 43,5 | - | - | 41,2 | 39,8 | 86 | 7,1 | 28,0 | 35,0 | - | - | 34,0 | 31,3 |
| 82 | - | - | 43,0 | - | - | 39,0 |  | 90 | 6,0 | 27,0 | 35,0 | - | - | 32,0 | 30,2 |
| 84 | - | - | 42,0 | 35,4 | - | 37,0 | - | 91 | , | , | 34,5 | - | - | 31,0 | 29,9 |
| 86 | - | - | 41,0 | 35,4 | - | 35,0 | - | 92 | - | - | 34,0 | 26,5 | - | 30,0 | - |
| 90 | - | - | 40,0 | 35,1 | - | 34,0 | - | 94 | - | - | 34,0 | 26,5 | - | 28,0 | - |
| 94 | - | - | 39,0 | 34,2 | - | 32,0 | - | 98 | - | - | 33,0 | 26,5 | - | 25,0 | - |
| 98 | - | - | - | 33,1 | - | 28,0 | - | 102 | - | - | 31,0 | 26,1 | - | 24,0 | - |
| 102 | - | - | - | 31,4 | - | 25,0 | - | 104 | - | - | 24,7 | 25,8 | - | 23,5 | - |
| 106 | - | - | - | 29,6 | 22,9 | 22,0 | - | 106 | - | - | - | 25,5 | - | 23,0 | - |
| 110 | - | - | - | - | 21,5 | 20,0 | - | 110 | - | - | - | 24,7 | - | 20,0 | - |
| 114 | - | - | - | - | 20,2 | 17,0 | - | 114 | - | - | - | 23,7 | - | 18,0 | - |
| 118 | - | - | - | - | 19,0 | 15,0 | - | 116 | - | - | - | 23,3 | 17,3 | 16,5 | - |
| 120 | - | - | - | - | 18,4 | 13,5 | - | 118 | - | - | - | 22,8 | 16,7 | 15,0 | - |
| 122 | - | - | - | - | , | 12,0 | - | 122 | - | - | - | - | 15,6 | 13,0 | - |
| 126 | - | - | - | - | - | 10,0 | - | 126 | - | - | - | - | 14,5 | 11,0 | - |
| 130 | - | - | - | - | - | 7,0 | - | 130 | - | - | - | - | 13,6 | 9,0 | - |
| 134 | - | - | - | - | - | 5,0 | - | 132 | - | - | - | - | 13,2 | 7,5 | - |
|  |  |  |  |  |  |  |  | 134 | - | - | - | - | - | 6,0 | - |
|  |  |  |  |  |  |  |  | 138 | - | - | - | - | - | 4,0 | - |

Main boom angle $85^{\circ}, 75^{\circ}, 65^{\circ}$ and $55^{\circ}$; capacities for intermediate boom positions are calculated by the crane control system IC-1
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| 1- -1.40 m |  |  |  | 11-15 m |  | $19.8 \mathrm{~m} / \mathrm{s}$ |  |  | $360^{\circ}$ |  |  | EN13000 / ISO |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $96 \mathrm{~m}+36 \mathrm{~m}$ |  |  |  |  |  |  |  | $96 \mathrm{~m}+48 \mathrm{~m}$ |  |  |  |  |  |  |  |
| $\bigcup_{1}$ |  | SWSL |  |  | $\text { SFSL } \stackrel{\text { HSWSL }}{\stackrel{\text { ST }}{ }}$ |  |  | $\begin{aligned} & \models \frac{0 t}{} \\ & 180 \mathrm{t}+ \\ & 60 \mathrm{tZB} \\ & 85^{\circ} \end{aligned}$ |  | SWSL |  |  |  | SFSL | $\begin{aligned} & \text { HSWSL } \\ & \quad-\mathrm{S} 7 \end{aligned}$ |
|  |  | $0 \mathrm{t}-250 \mathrm{t}$ |  |  |  |  |  |  |  | $0 \mathrm{t}-250 \mathrm{t}$ |  |  |  |  |  |
|  |  | 160 t |  |  |  |  |  |  |  | 160 t |  |  |  |  |  |
|  |  | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $55^{\circ}$ |  | $85^{\circ}$ |  |  | $85^{\circ}$ | $75^{\circ}$ | $65^{\circ}$ | $55^{\circ}$ |  | $85^{\circ}$ |
| m | t | t | t | t | t | t | t | m | t | t | t | t | t | t | t |
| 24 | 78,5 | 81,0 | - | - | - | - | 99,5 | 27 | - | - | - | - | - | - | 76,5 |
| 26 | 78,5 | 81,0 | - | - | - | 80,0 | 98,0 | 28 | 60,5 | 60,5 | - | - | - | - | 76,5 |
| 28 | 74,5 | 77,5 | - | - | - | 79,5 | 95,5 | 30 | 60,5 | 60,5 | - | - | - | 61,5 | 75,5 |
| 30 | 68,0 | 75,0 | - | - | - | 78,5 | 92,5 | 34 | 55,5 | 57,0 | - | - | - | 60,5 | 72,0 |
| 34 | 57,0 | 70,0 | - | - | - | 76,5 | 87,0 | 38 | 47,5 | 54,0 | - | - | - | 59,0 | 68,5 |
| 38 | 49,2 | 65,5 | - | - | - | 74,5 | 81,5 | 42 | 41,0 | 51,0 | - | - | - | 58,0 | 65,0 |
| 42 | 42,8 | 62,0 | - | - | - | 72,0 | 76,5 | 46 | 35,9 | 48,6 | - | - | - | 56,0 | 61,5 |
| 45 | - | - | - | - | - | 70,1 | 73,0 | 50 | 31,6 | 46,2 | - | - | - | 54,0 | 58,5 |
| 46 | - | - | 67,5 | - | - | 69,5 |  | 52 | 29,8 | 45,0 | 52,0 | - | - | 53,2 | 56,7 |
| 50 | - | - | 65,5 | - | - | 66,5 | - | 54 | 28,1 | 43,8 | 52,0 | - | - | 52,5 | 55,0 |
| 54 | - | - | 62,0 | - | - | 64,0 | - | 57 | - | - | 50,5 | - | - | 50,6 | 53,0 |
| 58 | - | - | 59,0 | - | - | 62,0 | - | 58 | - | - | 50,0 | - | - | 50,0 | , |
| 62 | - | - | 54,5 | - | - | 60,0 | - | 62 | - | - | 48,0 | - | - | 49,0 | - |
| 66 | - | - | - | - | - | 58,0 | - | 66 | - | - | 46,0 | - | - | 47,0 | - |
| 68 | - | - | - | 52,5 | - | 57,0 | - | 70 | - | - | 43,0 | - | - | 46,0 | - |
| 70 | - | - | - | 51,5 | - | 56,0 | - | 74 | - | - | 41,0 | 40,5 | - | 44,0 | - |
| 74 | - | - | - | 48,1 | - | 50,0 | - | 78 | - | - | , | 39,4 | - | 43,0 | - |
| 78 | - | - | - | 44,3 | - | 44,7 | - | 82 | - | - | - | 37,0 | - | 41,0 | - |
| 82 | - | - | - | - | - | 39,9 | - | 86 | - | - | - | 34,6 | - | 36,7 | - |
| 86 | - | - | - | - | 35,8 | 35,5 | - | 88 | - | - | - | 33,3 | - | 34,7 | - |
| 90 | - | - | - | - | 33,6 | 31,6 | - | 90 | - | - | - | - | - | 32,7 | - |
| 92 | - | - | - | - | 32,6 | 29,8 | - | 94 | - | - | - | - | - | 29,0 | - |
| 94 | - | - | - | - | - | 28,0 | - | 96 | - | - | - | - | 27,9 | 27,3 | - |
| 98 | - | - | - | - | - | 24,7 | - | 98 | - | - | - | - | 27,0 | 25,7 | - |
| 102 | - | - | - | - | - | 21,4 | - | 102 | - | - | - | - | 25,4 | 22,6 | - |
| 106 | - | - | - | - | - | 17,8 | - | 104 | - | - | - | - | 24,7 | 21,2 | - |
| 110 | - | - | - | - | - | 14,3 | - | 106 | - | - | - | - | - | 19,8 | - |
| 114 | - | - | - | - | - | 10,8 | - | 110 | - | - | - | - | - | 16,8 | - |
| 118 | - | - | - | - | - | 7,8 | - | 114 | - | - | - | - | - | 13,7 | - |
|  |  |  |  |  |  |  |  | 118 | - | - | - | - | - | 10,7 | - |
|  |  |  |  |  |  |  |  | 122 | - | - | - | - | - | 7,8 | - |
|  |  |  |  |  |  |  |  | 126 | - | - | - | - | - | 4,9 | - |

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[^0]:    Main boom angle $85^{\circ}, 75^{\circ}, 65^{\circ}$ and $55^{\circ}$; capacities for intermediate boom positions are calculated by the crane control system IC-1
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